

# Aircraft Avoidance Technologies

Tom Murphy  
UCSD

plus

E. Adelberger, J. Battat, **W. Coles**, C.D. Hoyle, K. Kassabian,  
R. McMillan, **J. Melser**, E. Michelsen, C. Stubbs, H. Swanson,  
**J. Tu**, A. White

# Agency Compliance & Headaches

- For APOLLO, we must interface with **four** agencies for safety compliance
  - **FAA** (Federal Aviation Administration)
  - Holloman Air Force Base
  - White Sands Missile Range
  - Space Command (satellites)
- The **FAA** requires **two human spotters** with eyes on the sky, blocking the laser if an aircraft comes within **25°** of the beam, or if the sky is obscured by clouds within **25°** of the laser beam
  - spotters are **difficult to schedule** in remote areas
  - sometimes they **get sick** or don't set their alarm correctly
  - spotters demand a continual cash-flow for **payment**
  - spotters do not have perfect **attention** and visual **reliability**
- **Radar systems** can be unwelcome at an observatory due to the high power RF interfering with other equipment

# Two Complementary Technologies

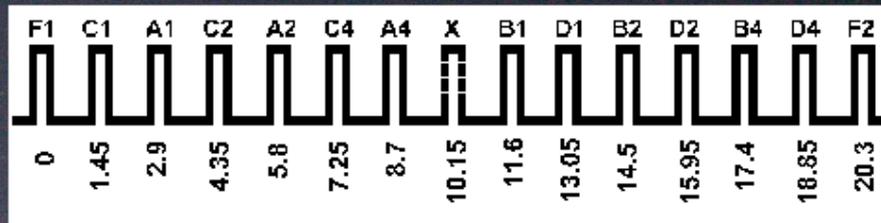
- APOLLO has chosen to explore **infrared** and **RF transponder** technologies for aircraft avoidance
- **Infrared (IR)** camera with motion-sensing software algorithm
  - works well for nearby (**< 5 km**) aircraft
  - works for low aircraft in radar shadow (low → close)
  - works for low-flying aircraft not required to have transponder
- **RF Transponder Detector** seeks 1090 MHz signal directionally
  - all aircraft above 10,000 ft (3,048 m: our observatory is at 9,200 ft) must have a transponder, unless within 2,500 ft (762 m) of surface
  - transponder transmissions are strong enough to detect very far away (**> 100 km**)
  - system is passive: transponder is continuously interrogated by ground radar systems, and the response is omni-directional: we just listen

# IR Camera Details

- Camera, lens, and software produced by Image Labs International, in Bozeman, Montana, USA
- Thermal infrared sensor sees  $\sim 300$  °K skin of aircraft against cold sky (effective sky temp at  $8\text{--}10$   $\mu\text{m}$   $< 100$  °K)
- Field of View is  $5^\circ \times 7^\circ$ , operating at video rate of 30 frames per second
- Worst-case angular velocity: aircraft traveling 100 m/s (360 kph; 220 mph) at range of 150 m travels  $1.3^\circ$  per frame period
  - software looks for 3 consecutive detections along a line to raise flag
  - worst-case still shuts laser in time
- Installed on telescope and running at APO, though currently bypassed and collecting data

# Transponder Basics

- Almost all aircraft carry transponders that respond to ground interrogations by sending out pulse train at **1090±3 MHz**
  - peak power must be **> 70 W**; **> 125 W** for commercial aircraft
  - pulse pattern carries information about either:
    - temporary aircraft identity (“squawk code”; called Mode-A)
    - encoded altitude (Mode-C)
  - depending on what the interrogator asks for (alternates)
  - pulse pattern consists of framing pulses plus **four 3-bit codes** for a total of 4096 combinations



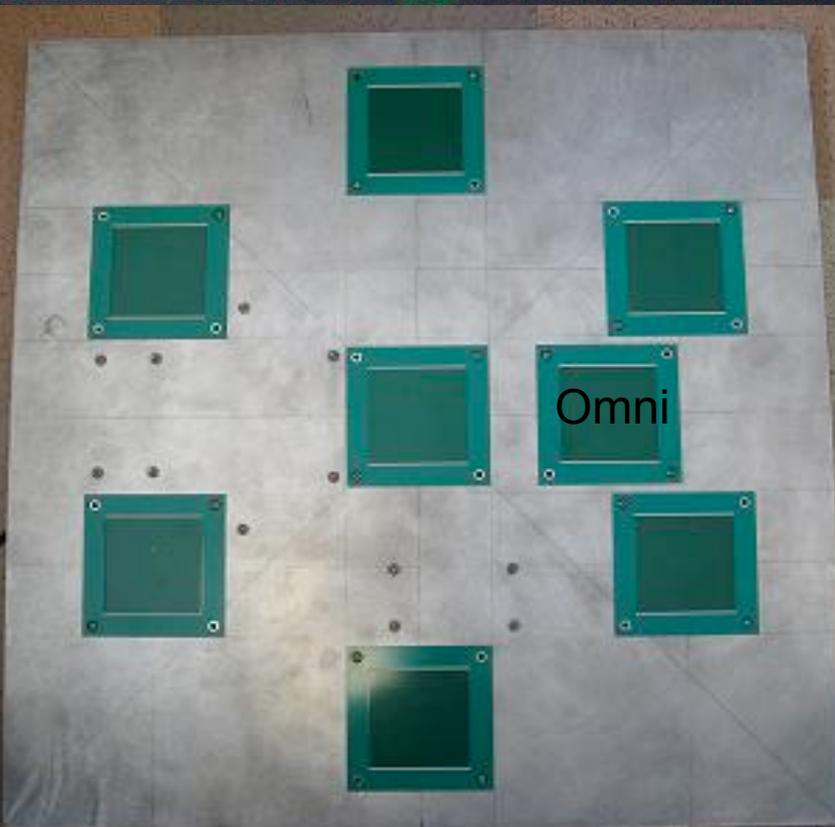
pulses 0.45 μs long, with pulse times given in μs. The F1 and F2 framing pulses are always present.

- The transponder signals are omni-directional, so all we need to do is determine if there is a source of 1090 MHz near our beam
  - aircraft also may emit strong DME signals near 1090 MHz, and these can leak into our receiver

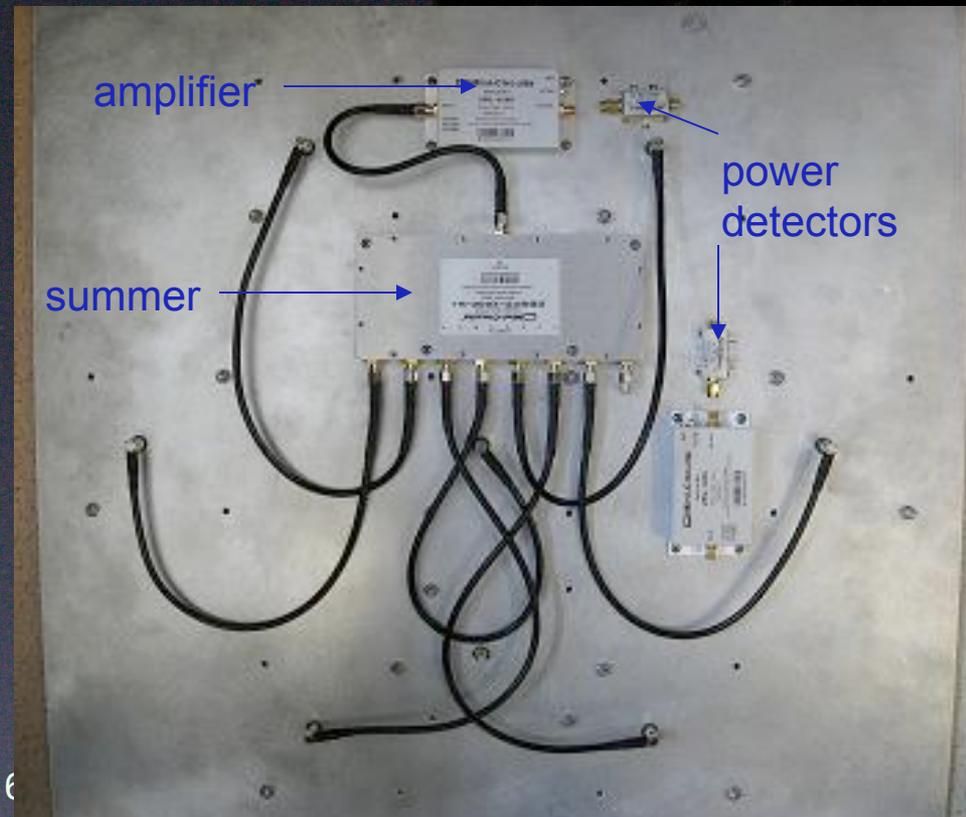
# Patch Antenna Array

- Directional sensitivity can be accomplished via a phased array of patch antennas
  - thin patches are inherently narrowband (1% in our case)
- ~7 cm patches on 10 cm boards are arranged into a 7-element array spanning ~0.6 m, plus a separate single (OMNI) patch

Front

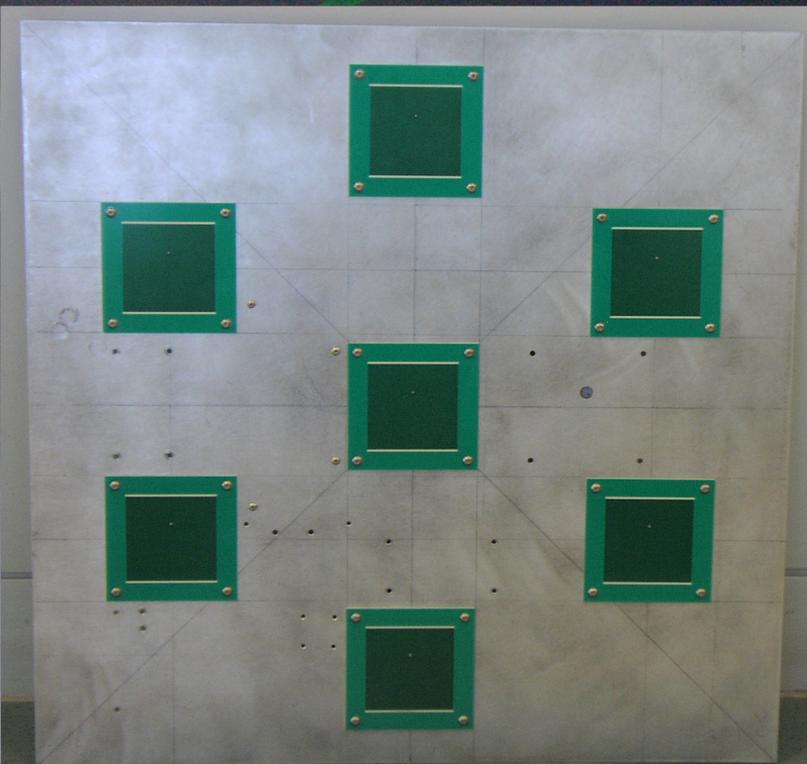
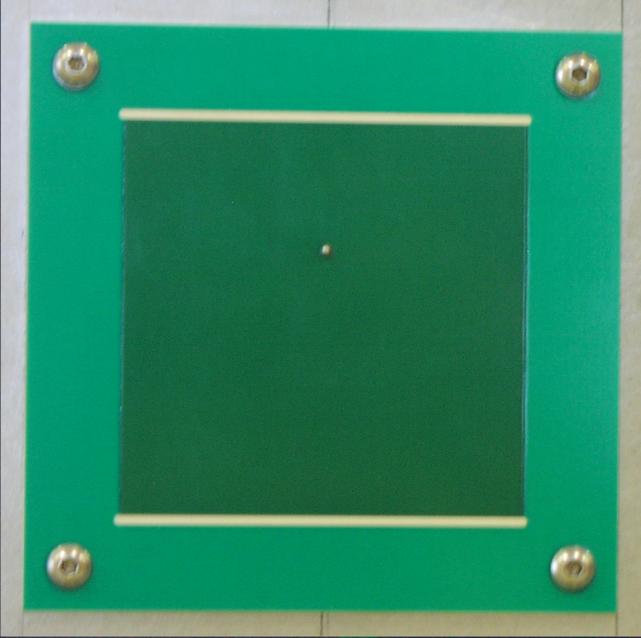


Back



# Alternate Scheme

- Can also use splitter on central element to double as omni-directional antenna
- Must then attenuate each perimeter element by 3dB to maintain beam pattern
- Advantage is elimination of parasitic coupling between array and omni antennae



center feed

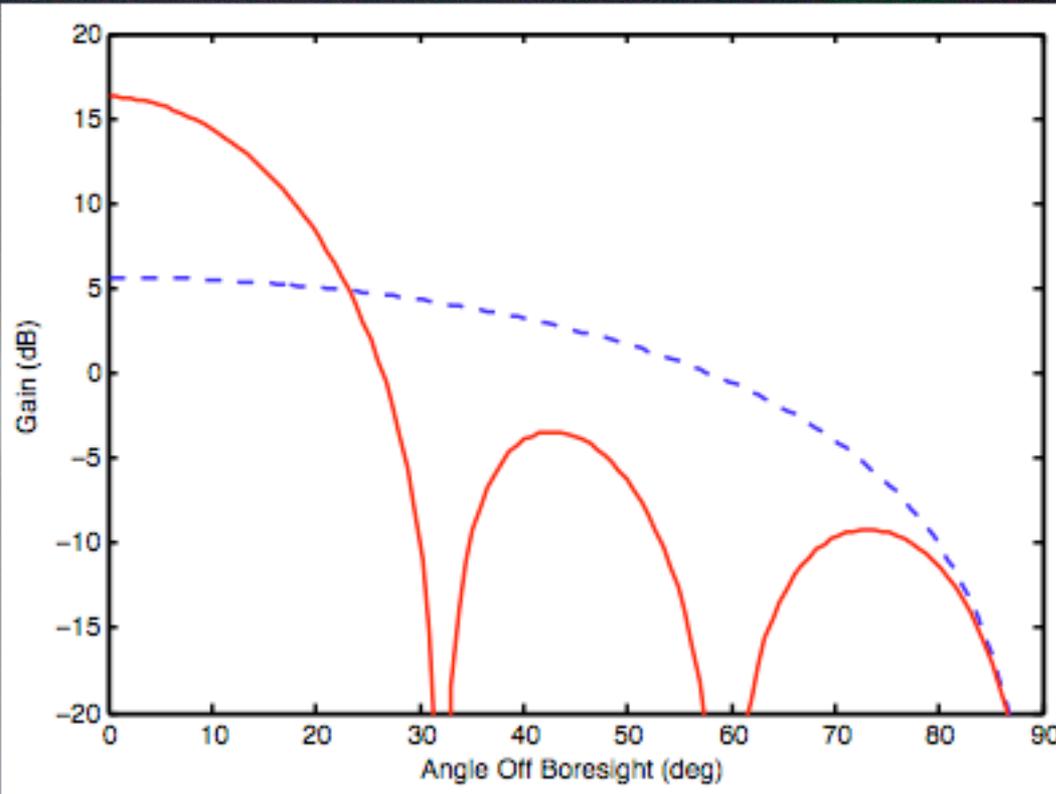
splitter

omni output  
array output

summer

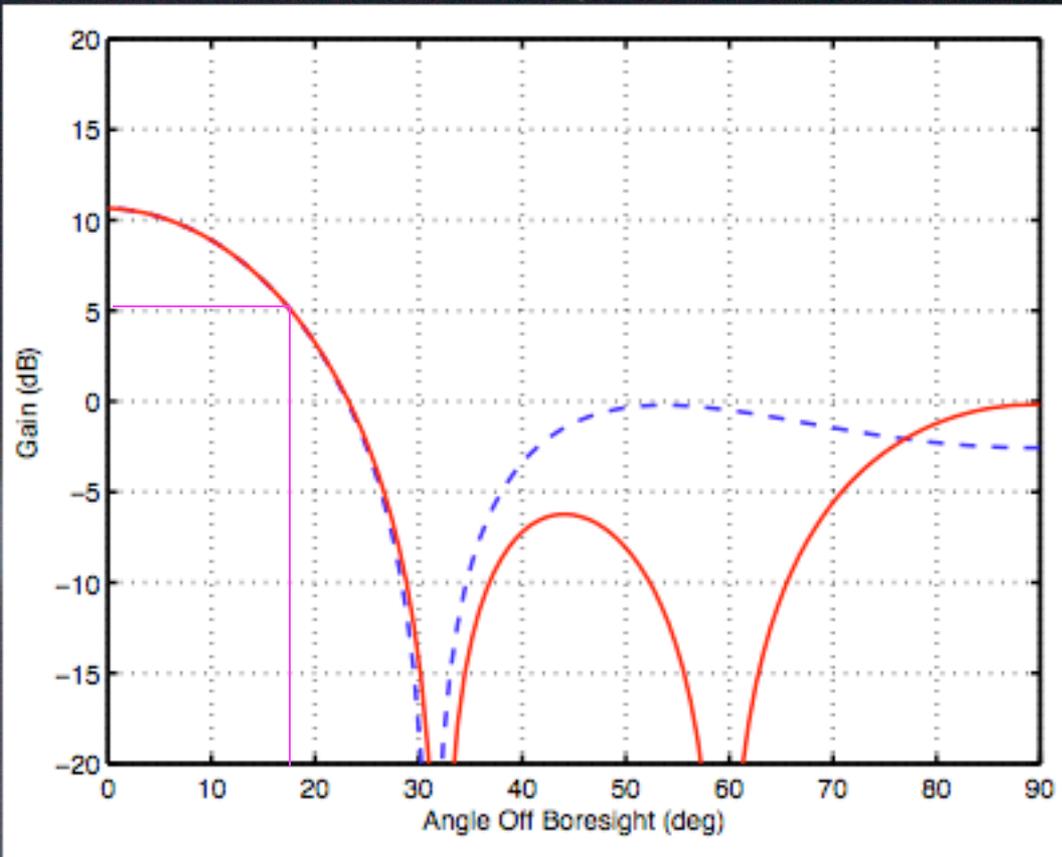
3dB attenuators

# Beam Patterns



- An individual patch is relatively omni-directional (blue curve)
- The phased array of 7 patches has much higher gain on boresight, and sidelobes elsewhere (red curve)
- The difference at beam center is  $11 \text{ dB} = 10^{1.1} = 13\times$
- Note that the single (omni) patch is always higher than the array sidelobes, but not the main directional beam

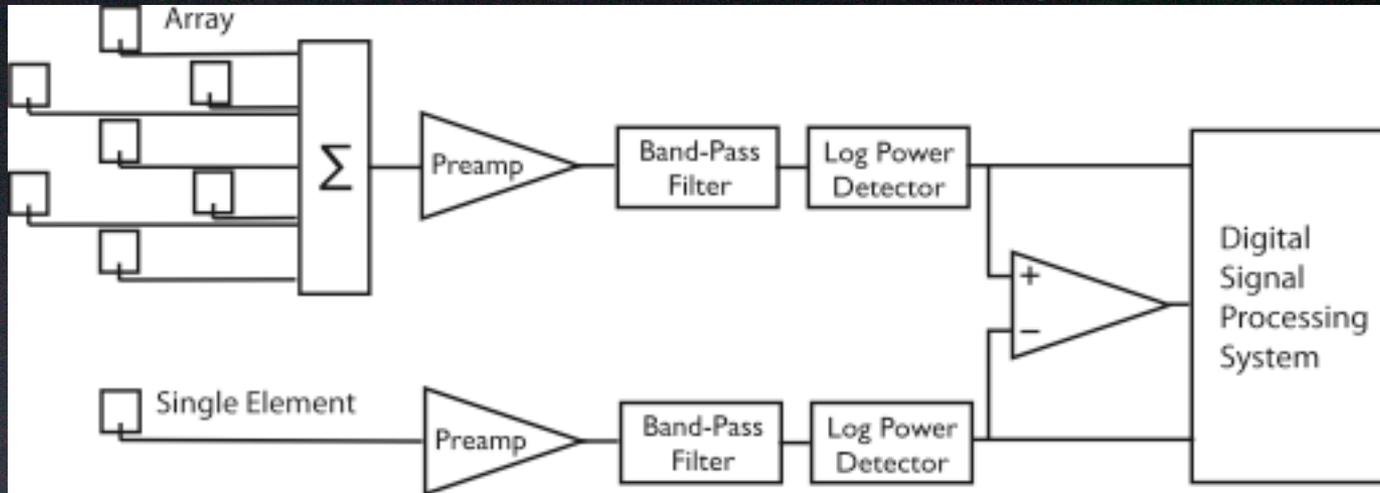
# The Ratio is the Key



Example: set ratio criterion at 5 dB, and the beam half-width becomes 18°

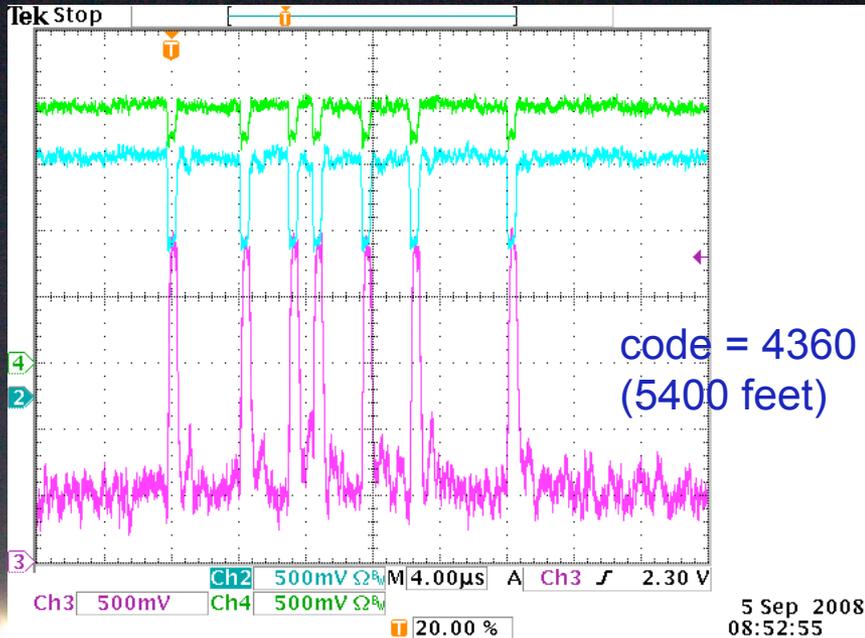
- The **ratio** between the directional signal and the omni-directional patch signal is shown at left
- **Red** and **blue** curves represent two different azimuthal cuts with respect to the hexagonal array pattern
- For both cuts, the sidelobes are always  $< 0$  dB
- The peak is 11 dB, as we saw previously
- By using the **ratio** as the criterion, **we are immune to distance, power, and polarization variables**

# Implementation

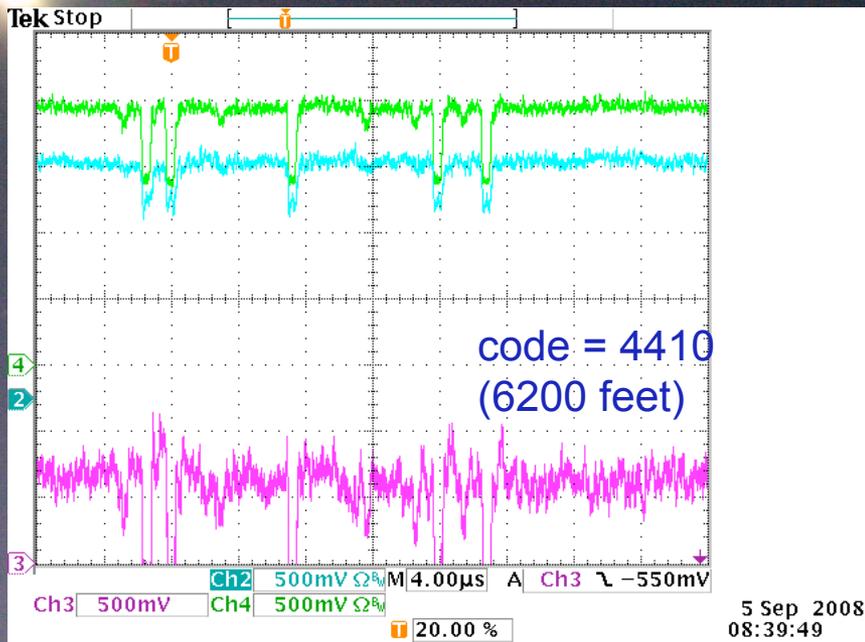


- The array elements are summed, then both array and omni signals are amplified, filtered, then passed to a **logarithmic power detector**
  - thus **voltage difference is array/omni ratio**
- Decisions are made based on the difference signal, and also on the raw power levels:
  - DIFF** > **thresh<sub>1</sub>** → in the primary beam
  - ARRAY** < **saturation** → otherwise DIFF not reliable
  - OMNI** < **thresh<sub>2</sub>** → if OMNI that hot, shut down for nearby plane
- Also processor **decodes** pulse train, and presents for logging

# Example Pulse Patterns

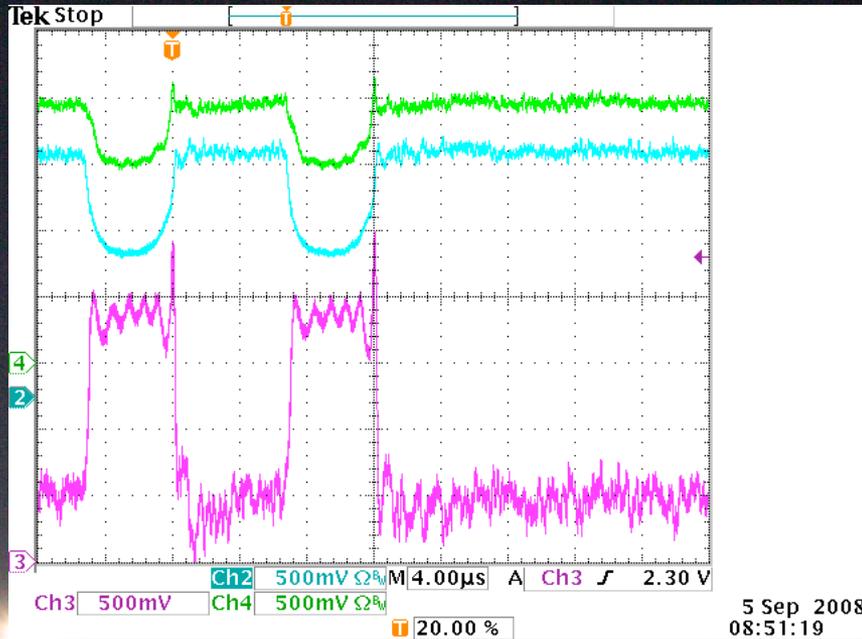


- $ARRAY > OMNI$ , so  $DIFF$  is large (in beam)
  - note raw signals for  $OMNI$  and  $ARRAY$  are negative-going: negative dips are the signal pulses
- A threshold on the  $DIFF$  signal alerts the system that a plane is in the beam

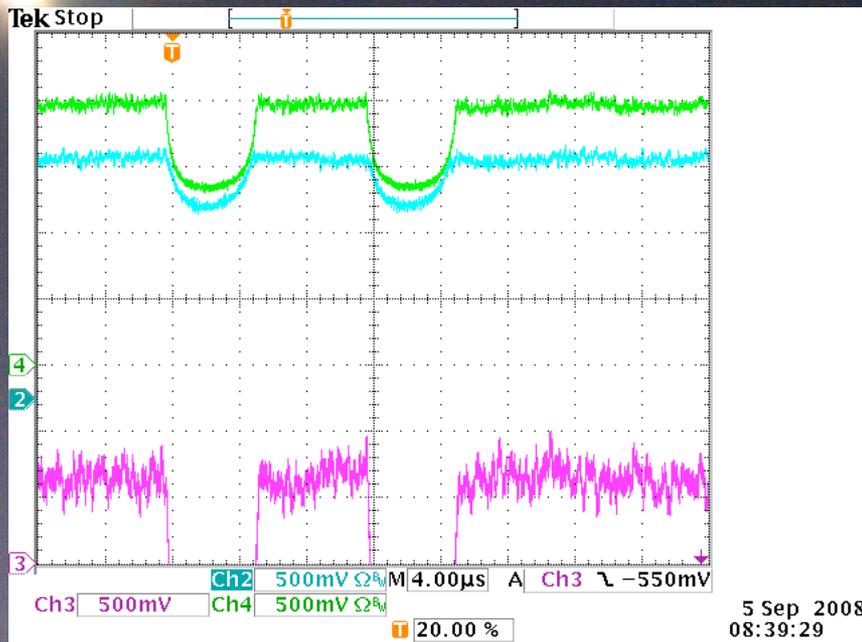


- $ARRAY < OMNI$ , so  $DIFF < 0$ 
  - thus while signals are present, the  $DIFF < 0$  indicates that the plane is not in the main beam

# DME signal works too...

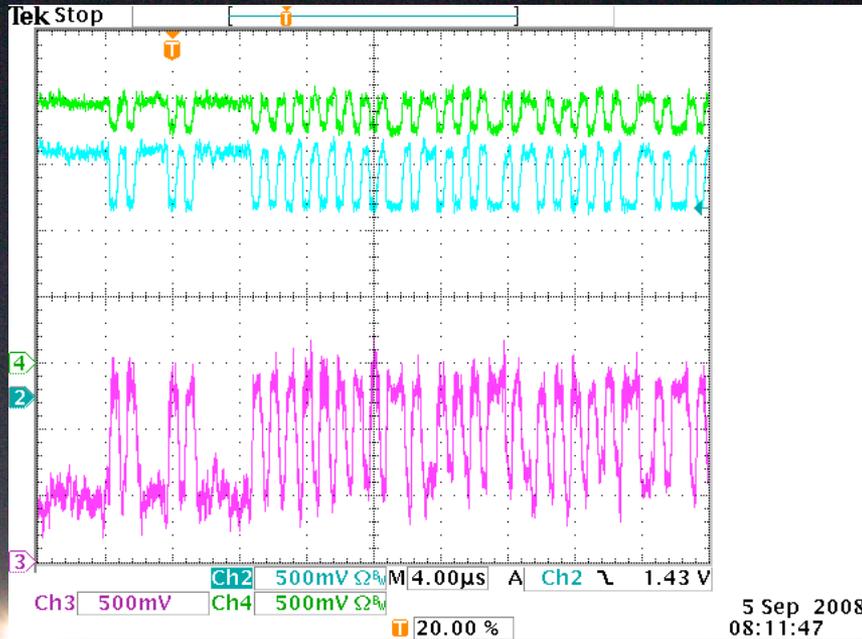


- ARRAY > OMNI, so DIFF is large (in beam)
- A threshold on the DIFF signal alerts the system that a plane is in the beam
- Note the flatness of the DIFF signal: the ratio works!

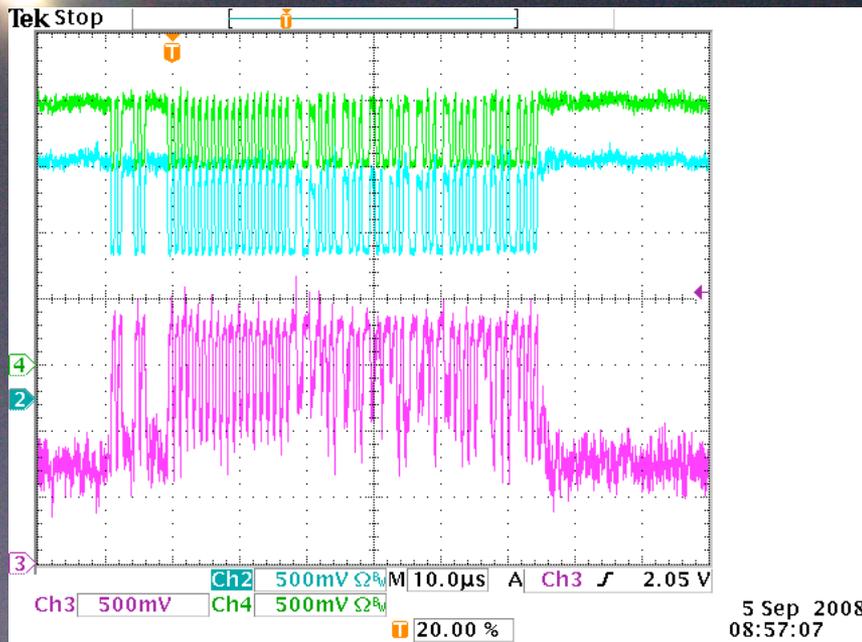


- ARRAY < OMNI, so DIFF < 0
  - thus while signals are present, the DIFF < 0 indicates that the plane is not in the main beam
- Though DME  $\neq$  transponder, who cares?! It's still an airplane

# Mode-S transmission



- A new coding of information is sweeping the 1090 airwaves: Mode-S
- Mode-S carries permanent aircraft identity, and higher-precision altitude information
- The **top** plot is at the same time-scale as the previous plots, but to get the whole thing, we have to zoom out (**below**)
- All the same, these signals trigger the system if the source is in the beam



# What Happens Next?

- The prototype is **working** at UCSD, with a few upgrades in the works
  - one such upgrade is splitting the central element to double-task it with the job of being the OMNI antenna — compactifying the arrangement
- Once deployed, we will begin **logging** data whenever the dome is open, so we build a case to present to the FAA
- Same goes for the IR camera
- Once verified and (hopefully) accepted, we will be able to **shed the spotters**
  - we may get help from the Keck, Palomar, and Lick observatories (among others?) as all are currently using spotters in conjunction with their laser guide star adaptive optics programs